

TURCK

Your Global Automation Partner

IM1... | MK13-R-EX0 Isolating Switching Amplifier

Safety manual



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1 About this safety manual

This safety manual contains regulations for the use of the devices in safety instrumented systems (SIS). The consideration of safety-relevant values is based on IEC 61508. The safety manual describes the values determined for SIL assessment and is only valid in conjunction with the attached EXIDA report FMEDA Turck 04/07-14 R002. Read this document carefully before using the device. This will prevent the risk of personal injury or damage to property or equipment. Keep the safety manual in a safe place as long as the device is in use. If the device is passed on, pass on this safety manual as well.



DANGER

Malfunction due to operator error

Risk of death due to failure of the safety function!

- ▶ It is essential to comply with the regulations contained in this safety manual when using the device in safety-related applications.
-

1.1 Target groups

The safety manual is intended for specialist personnel or trained personnel. It must be read and understood by any person responsible for any of the following:

- Unpacking and mounting
- Commissioning
- Inspection and maintenance
- Troubleshooting
- Dismantling and disposal

1.2 Explanation of symbols

The following symbols are used in these instructions:



DANGER

DANGER indicates an imminently hazardous, high-risk situation which, if not avoided, will result in death or serious injury.



NOTE

NOTE indicates tips, recommendations and important information. The notes will facilitate work, provide more information on specific actions and help prevent additional work due to incorrect processes.



CALL TO ACTION

This symbol denotes action steps that the user must carry out.



ACTION RESULT

This symbol denotes the relevant results of actions and action sequences.

1.3 Abbreviations and names

For definitions, see IEC 61508-4

DC	Diagnostic coverage	Diagnosedeckungsgrad
E/E/PE system	Electrical/electronic/programmable electronic system	elektrisch/elektronisch/programmierbares elektronisches System
EUC	Equipment under control	EUC setup
	Dangerous failure	gefährbringender Ausfall
	No effect failure	Ausfall ohne Auswirkung
	No part failure	Ausfall eines unbeteiligten Bauteils
	Safe failure	ungefährlicher Ausfall
	Safe state	sicherer Zustand
HFT	Hardware fault tolerance	Hardwarefehlertoleranz
	High demand mode	Betriebsart mit hoher Anforderungsrate
	Low demand mode	Betriebsart mit niedriger Anforderungsrate
MooN	M out of N channel architecture	Architektur mit M-aus-N Kanälen
MTBF	Mean time between failures	mittlere Betriebsdauer zwischen Ausfällen
MTTR	Mean time to restoration	mittlere Dauer bis zur Wiederherstellung
PFD	Probability of dangerous failure on demand	Wahrscheinlichkeit eines gefährbringenden Ausfalls bei Anforderung
PFD_{AVG}	Average probability of dangerous failure on demand	mittlere Wahrscheinlichkeit eines gefährbringenden Ausfalls bei Anforderung
PFH	Average frequency of a dangerous failure per hour	mittlere Häufigkeit eines gefährbringenden Ausfalls je Stunde
SFF	Safe failure fraction	Anteil sicherer Ausfälle
SIF	Safety instrumented function	Sicherheitsfunktion
SIS	Safety instrumented system	das sicherheitstechnische System
SIL	Safety integrity level	Sicherheits-Integritätslevel
	Proof test	Wiederholungsprüfung
	Proof test interval	Intervall für die Wiederholungsprüfung

1.4 Document history

Rev.	Description	Date
1.0.0	First edition	04/02/2015
2.0.0	Change to useful lifetime Layout changes	06/05/2024

The German version is considered the authoritative document. All translations have been prepared with great care. If you are unsure about how to interpret the manual, please use the German safety manual or contact Turck directly.



NOTE

Always use the latest version of the safety manual. Check if a newer version is available.

2 Information about the devices

2.1 Device variants

This safety manual is valid for the following Turck isolating switching amplifiers:

IM1-12Ex-R	IM1-22Ex-T
IM1-12Ex-T	IM1-121Ex-R
IM1-12-T	IM1-121Ex-T
IM1-22Ex-R	MK13-R-Ex0
IM1-22-R	

Scope of delivery

The device and the SIL registration card are included in the scope of delivery.

2.2 Turck service

Turck provides you with support and assistance for your projects — from the initial analysis to commissioning your application. The Turck product database at www.turck.com offers you several software tools for programming, configuring or commissioning, as well as data sheets and CAD files in many export formats.

Contact details for Turck branches worldwide can be found on p. 46.

3 For your safety

The device is designed in accordance with the latest standards. However, residual risks still exist. Observe the following warnings and safety information to prevent personal injury or damage to property. Turck accepts no liability for damage caused by failure to observe regulations.

3.1 Intended use

Isolating switching amplifiers are used for galvanically separated transmission of binary signals from sensors and mechanical contacts. You can also connect sensors in accordance with DIN EN 60947-5-6 (NAMUR) and mechanical contacts to them.

The output circuits are galvanically isolated from the input circuits and are designed either as relay outputs or potential-free transistor outputs.

The isolating switch amplifiers of the IM1-...Ex-... and MK13-R-Ex0 types have Ex approval and are used to transfer binary signals from Ex areas into safe areas.

These devices also enable the creation of safety-related systems up to and including SIL2 in accordance with IEC 61508; (hardware fault tolerance HFT = 0). The devices may only be used in safety-related circuits if all requirements arising from this safety manual and the EXIDA report are strictly adhered to. The information in the EXIDA report applies to applications with a low demand rate (device type A for low-demand operation) when IEC 61508 is used. When used in safety systems, the probability of failure (PFD) for the entire circuit must be determined and taken into account.

3.2 Obvious misuse

When using 2-channel devices in safety circuits, the second channel must not be used to increase hardware fault tolerance and thus achieve a higher SIL level.

The isolating switching amplifiers of type IM1-...Ex-... may be installed in Zone 2 in accordance with the ATEX Directive; the isolating switching amplifiers of type IM1-...-... and MK13-R-Ex0 may not be installed in hazardous areas as per the ATEX Directive.

3.3 SIL registration card



NOTE

In the case of safety-related applications of the devices, the SIL registration card supplied with the device must be filled out by the user and returned to TURCK.

3.4 General safety regulations

- The user is responsible for ensuring that the device is used in accordance with the applicable regulations, standards and laws.
- The suitability for specific applications must be assessed by considering the particular overall safety-related system with regard to the requirements of IEC 61508.
- Only trained personnel may mount and install the device.
- The device may only be commissioned and operated by experienced users.
- A function test must be carried out before initial operation, after each parameterization, after repair and replacement and at the specified time interval T[Proof]
- When operating the device, ensure that the power supply complies with the specified voltage range.
- Ensure that the plug connections and cables are always in good condition.
- Before use in the safety-related circuit, it must be checked whether the desired function has actually been set.
- Special application-specific influences, such as chemical and physical stresses, can lead to premature wear and tear of the devices and must be taken into account at the system planning stage; compensate for a lack of empirical values by taking special measures, e.g. by shortening inspection intervals.
- In the event of faults within the device that cause a transition to the state defined as safe, measures must be taken that maintain the safe state when the entire control system continues to be operated.
- Dangerous failures must be reported to TURCK without delay.
- A defective device must be replaced without delay and must not be repaired.
- Immediate replacement is necessary in the event of defective terminals or visible faults on the device.
- Tampering and modifications to the device are not permitted. Repairs may only be carried out by Turck. Send the device to Turck for this purpose (see the "Repair" section).
- The device must be secured against unintentional changes to its settings.
- Before using the product in safety-relevant applications, the information in this safety manual must always be checked for applicability to the application in question (e.g. to special industry-specific requirements and practices). In case of doubt, please contact the manufacturer at the address specified.

4 Device-specific information about safety applications

4.1 Safety function

Input signal evaluation:

- Depending on the input signal and the operating mode
 - the relay is de-energized (device with relay output)
 - the transistor is locked (device with transistor output)
- Wire break and short-circuit monitoring is part of the safety function. Wire break and short circuit lead to the output state LOW.



DANGER

The characteristic values determined apply to the use of an output in safety-relevant functions. In the case of signal duplication, the second output must not be used for the safety function.

Danger to life due to misuse!

- ▶ In the case of signal duplication, use only one output for the safety function.
-

4.2 Safe state

The safe state is defined in such a way that the output is LOW (relay is de-energized or transistor is disabled).

4.3 Functions and operating modes

The following characteristics characterize the isolating switching amplifiers with NAMUR input:

- Switching point: (1.55 ± 0.2) mA
- Current consumption in the event of a wire break: < 0.2 mA
- Current consumption in the event of short circuit: > 6 mA

4.3.1 Level switching

Level switching for 2-channel devices: A level change at the input causes a level change at the associated output.

4.3.2 Signal duplication

Signal duplication: A level change at the input of channel 1 causes a level change at both outputs.

4.3.3 Line monitoring

In the event of a wire break and short circuit, the associated output switches to LOW.

4.3.4 Error acknowledgment

Faults do not have to be acknowledged. If the error has been eliminated, the device automatically resumes operation.

4.4 Types of faults and failures

Faults related to the application must be classified into safe (non-dangerous) and unsafe (dangerous) errors. You as the operator are responsible for this.



NOTE

Any damage caused by a dangerous undetected failure must be reported to Turck immediately.

4.5 Safety-related parameters

4.5.1 FMEDA assumptions

The safety-related characteristic values were determined on the basis of an FMEDA according to IEC 61508. The FMEDA is based on the following assumptions:

- Failure rates are constant.
- Mechanical wear is not considered.
- Propagation of failures is not relevant.
- The mean time to repair (MTTR) after a non-hazardous fault is eight hours (replacement of the device).
- The device is operated in low demand mode.
- External power supply failure rates are not included.
- Only one input and one output are part of the safety function.
- The failure rates used are the Siemens SN 29500 standards at 40 °C.
- The second channel of a device cannot be used to increase the hardware fault tolerance HFT.
- The environmental conditions correspond to an average industrial environment defined in MIL-HNBK-217-F or IEC 60654-1, Class C (sheltered location).
 - The ambient temperature is usually 40 °C.
 - A safety factor of 2.5 must be applied at ambient temperatures of 60 °C and in the event of frequent temperature fluctuations.

4.5.2 Hardware architecture

The device is considered a type A component (non-complex device). The hardware fault tolerance HFT is 0.

4.5.3 Characteristic values for the MK13-R-Ex0 isolating switching amplifier

The device can be used for applications up to SIL 2.

$$MTBF = MTTF + MTTR = 1/(\lambda_{\text{total}} + \lambda_{\text{not part}}) + 8 \text{ h} = 279 \text{ years}$$

MK13-R-Ex0 — rate of non-dangerous and dangerous failures

λ_{safe}	$\lambda_{\text{dangerous}}$	SFF
288 FIT	110 FIT	72 %

MK13-R-Ex0 — mean failure probability in case of a request

T[Proof] = 1 year	T[Proof] = 5 years	T[Proof] = 10 years
PFD _{AVG} = 4.80 × 10 ⁻⁴	PFD _{AVG} = 2.40 × 10 ⁻³	PFD _{AVG} = 4.79 × 10 ⁻³

4.5.4 Characteristic values for IM1-...Ex-R

The devices are rated for applications up to SIL 2.
 MTBF = MTTF + MTTR = 1/(λ_{total} + λ_{not part}) + 8 h = 272 years

IM1-...Ex-R – rate of non-dangerous and dangerous failures

λ _{safe}	λ _{dangerous}	SFF
299 FIT	110 FIT	73 %

IM1-...Ex-R — mean failure probability in case of a request

T[Proof] = 1 year	T[Proof] = 5 years	T[Proof] = 10 years
PFD _{AVG} = 4.80 × 10 ⁻⁴	PFD _{AVG} = 2.40 × 10 ⁻³	PFD _{AVG} = 4.79 × 10 ⁻³

4.5.5 Characteristic values for IM1-...-Ex-T

The devices are rated for applications up to SIL 2.
 MTBF = MTTF + MTTR = 1/(λ_{total} + λ_{not part}) + 8 h = 314 years

IM1-...-Ex-T — rate of non-dangerous and dangerous failures

λ _{safe}	λ _{dangerous}	SFF
267 FIT	85 FIT	75 %

IM1-...-Ex-T — mean failure probability in the case of a request

T[Proof] = 1 year	T[Proof] = 5 years	T[Proof] = 10 years
PFD _{AVG} = 3.72 × 10 ⁻⁴	PFD _{AVG} = 1.86 × 10 ⁻³	PFD _{AVG} = 3.71 × 10 ⁻³



NOTE

The PFD_{AVG} value of the isolating switching amplifiers should be designed for a maximum of 10 % of the permissible PFD_{AVG} total value for safety integrity level SIL2. A PFD_{AVG} value with a green background indicates that the PFD share according to IEC 61508-1 is within the SIL2 range and is less than 10 % of the total value for SIL2. A PFD_{AVG} value with a yellow background indicates that the PFD component according to IEC 61508-1 is within the SIL2 range, but is more than 10 % of the total value for SIL2.

4.6 Recurring function tests

A function test must be carried out before first operation, after each parameterization, after repair and replacement and at the specified time interval T[Proof]:

- ▶ Ensure that the function test is only carried out by qualified personnel.
- ▶ Think first about your safety and the safety of your environment. If in doubt, replace the device.
- ▶ Bridge the isolating switching amplifier in the safety controller (PLT) and ensure that safety remains assured. You as the operator are responsible for ensuring safety.
- ▶ Simulate a short circuit at the input and check if the outputs change to LOW.
- ▶ Simulate a wire break at the input and check whether the outputs change to LOW.
- ▶ Simulate a switching operation at the input and check whether the corresponding output behaves according to the desired parameterization.
- ▶ Once all tests have been completed and no faults have been detected, restart the safety circuit.
- ▶ Document and archive the results after performing the test.



NOTE

The function test reveals more than 90 % of the unrecognized dangerous faults (Du) of the device.

4.7 Useful lifetime

Experience has shown that the useful lifetime often lies within a range of 8 to 12 years. It can be significantly less if elements are operated near their specification limits. However, the useful lifetime can be extended by appropriate measures. For example, heavy temperature fluctuations could potentially reduce the device's useful lifetime. Constant temperatures below 40 °C may help to increase it.

For the relay outputs ($\cos \phi = 1, I = 2 \text{ A/AC}$) the useful lifetimes is 8 to 12 years or 50,000 switching cycles.

4.8 Special regulations and restrictions



NOTE

Each application has its own specific operating and environmental conditions. Therefore, in addition to the general statements on failure probabilities, tolerances and failure rates of the components, the specific process must always be considered when assessing the safety of a system. For example, special chemical and physical stresses can lead to premature wear and tear of the devices, the influences of which must be taken into account during system planning. Compensate for a lack of empirical values by taking special measures, e.g. by shortening inspection intervals. The assessment of the diagnostic coverage (DC) may vary from application to application. Hardware fault tolerance (HFT) can only be assessed if restrictions are made on the application of the compliant object.

5 Installation and commissioning



DANGER

Malfunction due to errors during commissioning and operation

Risk of death due to failure of the safety function!

- Ensure that the product is mounted, installed, operated and serviced only by trained and experienced personnel.

5.1 Installing

Observe the installation instructions within the instructions for use.

5.2 Connection

Observe the installation instructions in the operating instructions.

5.2.1 Wiring diagrams

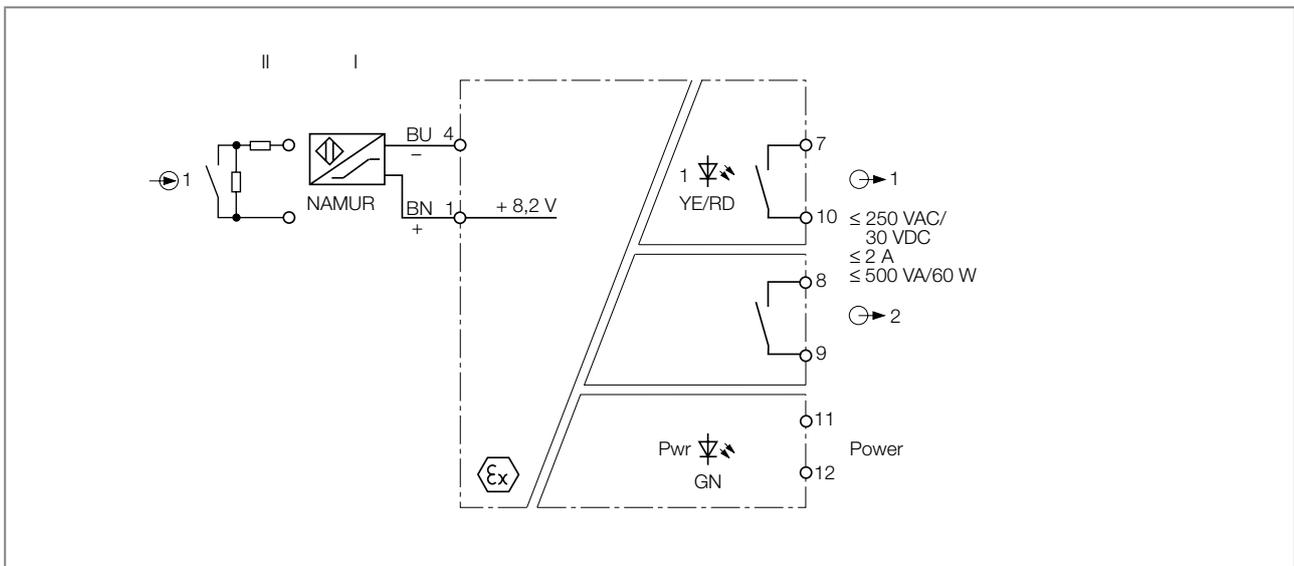


Fig. 1: Block diagram IM1-12Ex-R

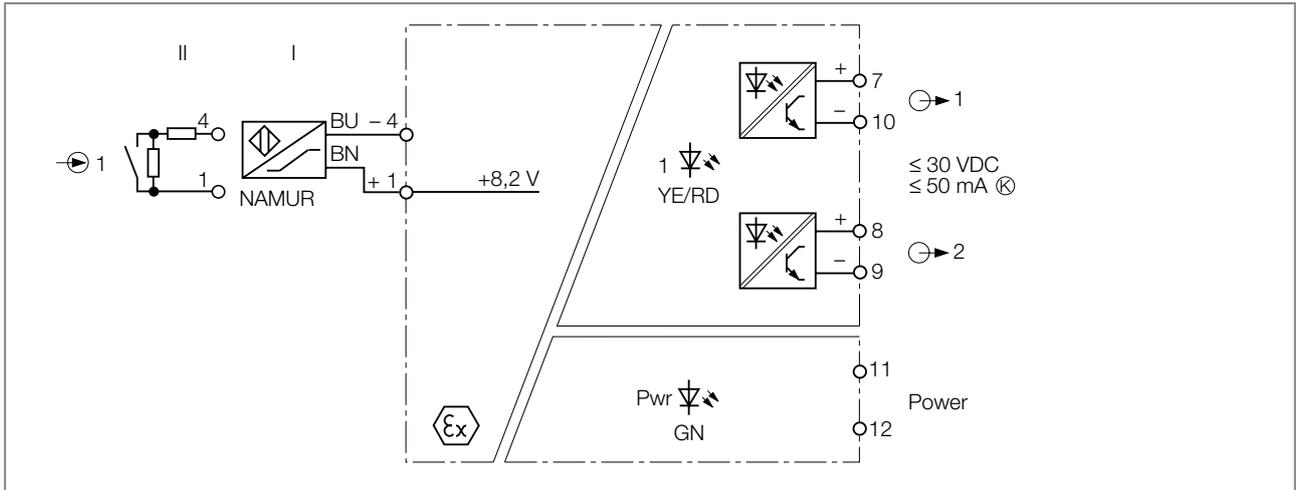


Fig. 2: Block diagram IM1-12Ex-T

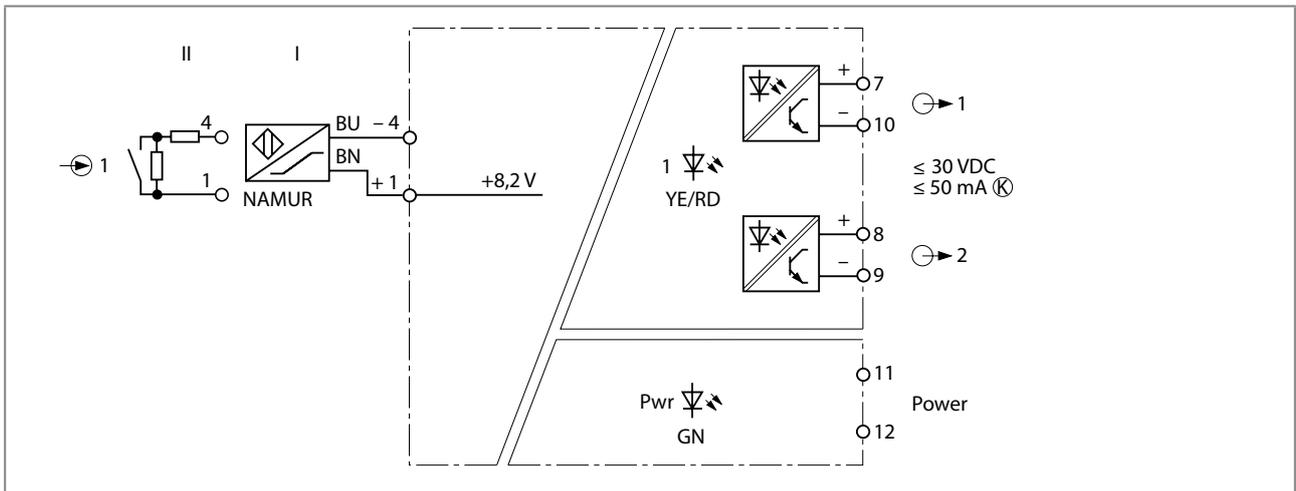


Fig. 3: Block diagram IM1-12-T

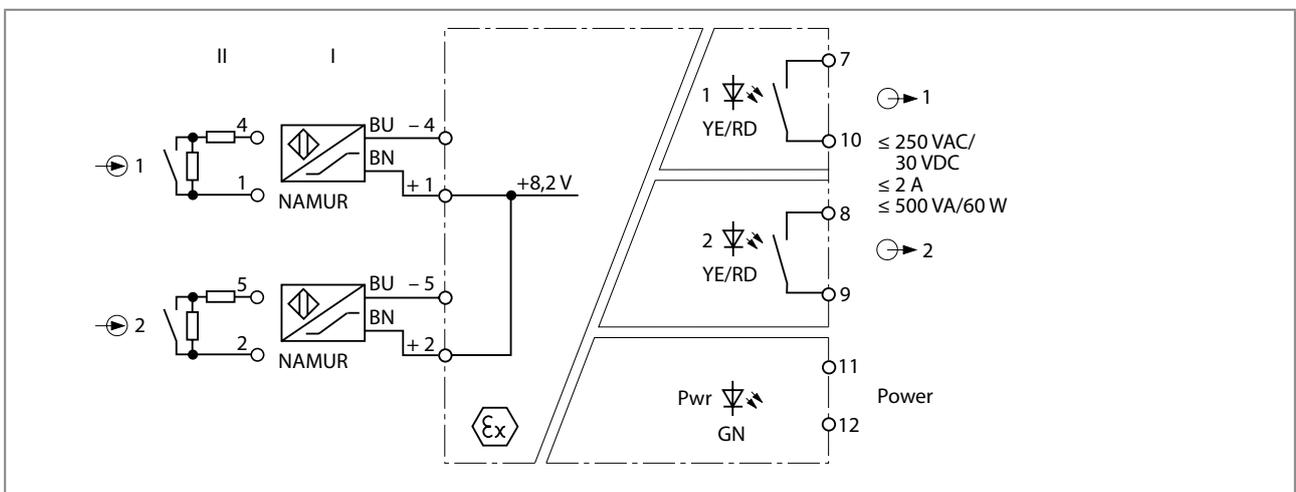


Fig. 4: Block diagram IM1-22Ex-R

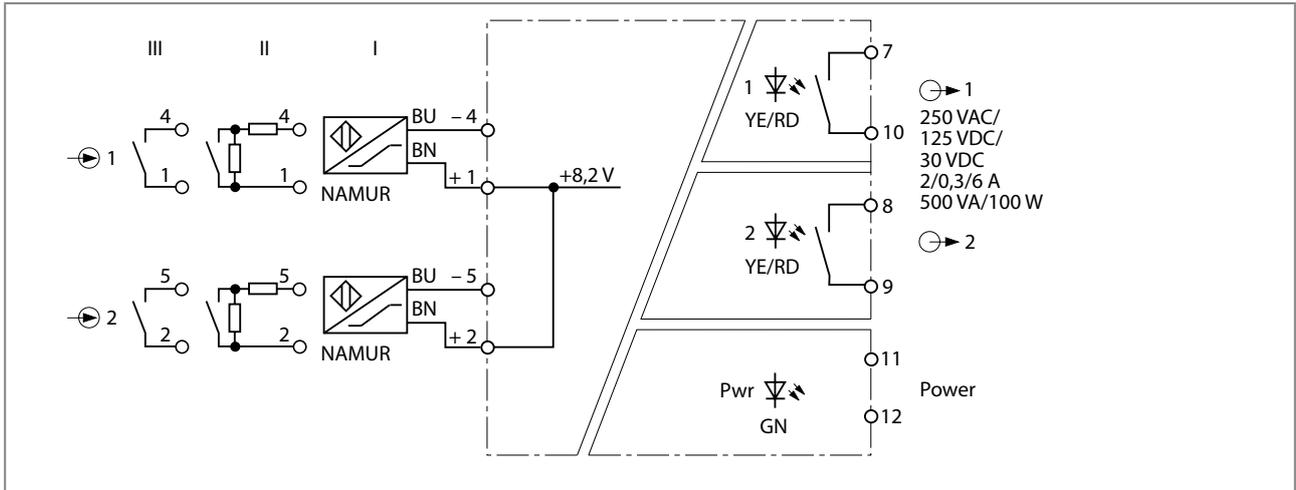


Fig. 5: Block diagram IM1-22-R

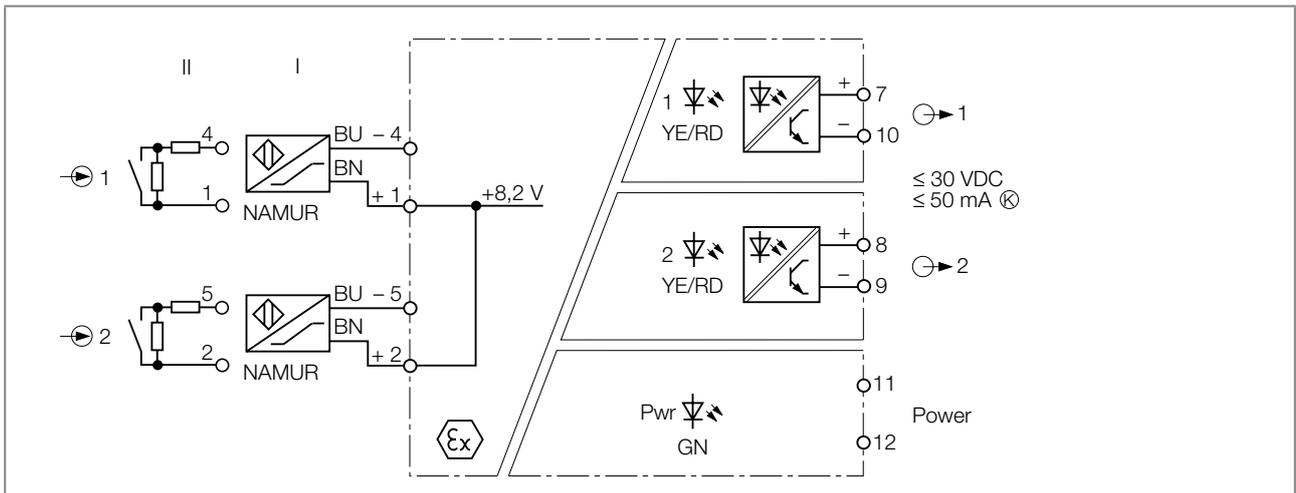


Fig. 6: Block diagram IM1-22Ex-T

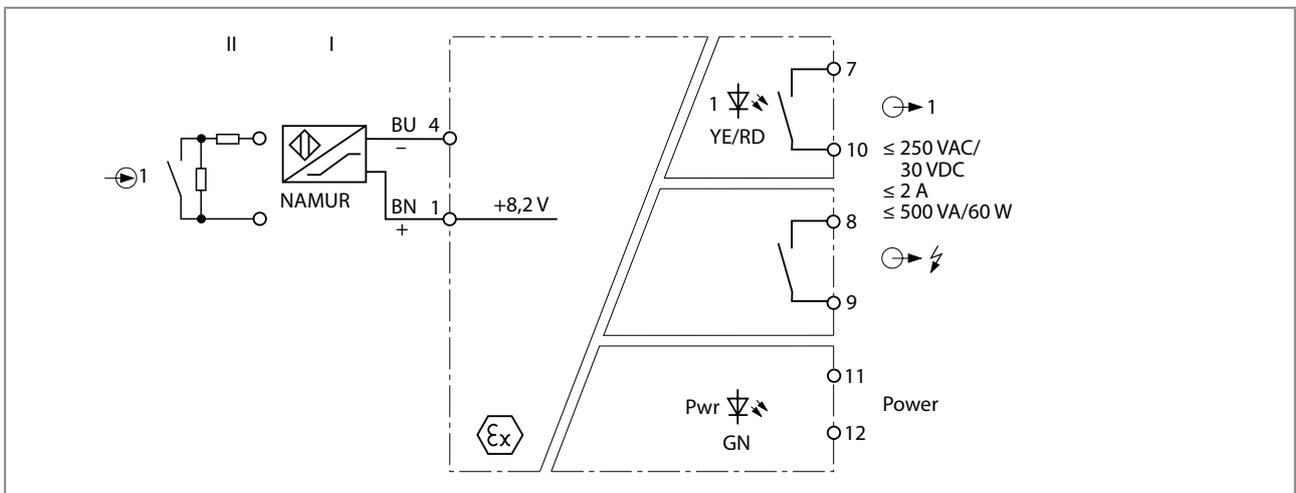


Fig. 7: Block diagram IM1-121Ex-R

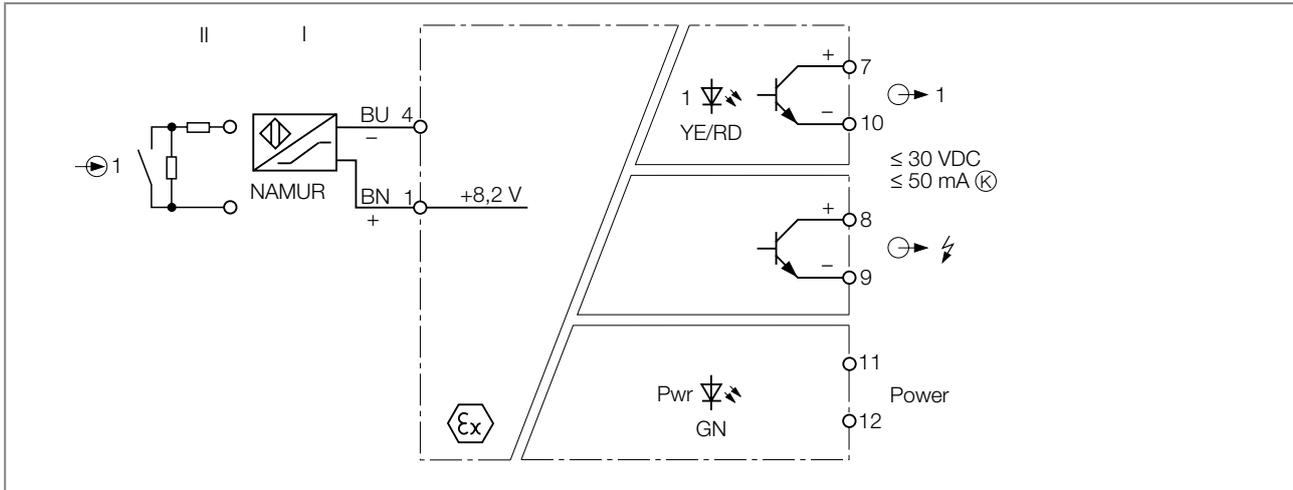


Fig. 8: Block diagram IM1-121-Ex-T

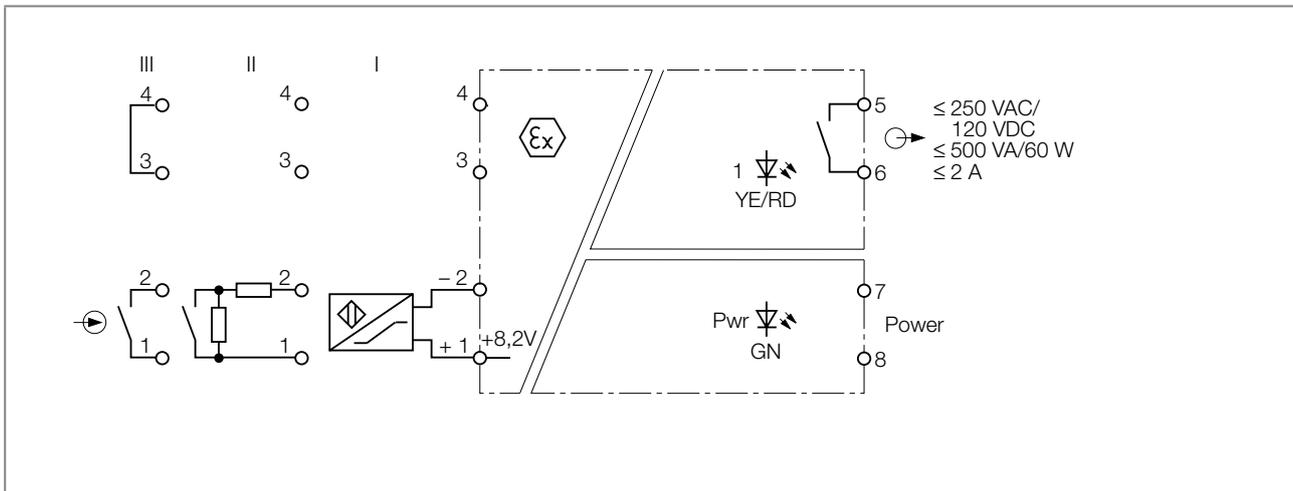


Fig. 9: Block diagram MK13-R-Ex0

5.3 Commissioning

When operating the device, ensure that the power supply complies with the specified voltage range. Commissioning is described in the instructions for use of the respective device.



DANGER

Malfunction due to operating and device errors

Risk of death due to failure of the safety function!

- ▶ Perform a T[Proof] function test before first operation, after each parameterization, after repair and replacement and at the specified interval.

5.3.1 Selecting sensors

If sensors according to EN 60947-5-6:2000 are used in safety circuits, the sensors must be certified according to IEC 61508.

Make sure that the devices and the housing materials are suitable for the application in question.

You can also find out more about this in the relevant data sheets of the Turck devices at www.turck.com.

5.3.2 Selecting mechanical contacts

If mechanical contacts are used in safety circuits, the contacts must be certified in accordance with IEC 61508.

5.4 Parameterization



DANGER

Malfunction due to operating and device errors

Risk of death due to failure of the safety function!

- ▶ Perform a T[Proof] function test before first operation, after each parameterization, after repair and replacement and at the specified interval.



DANGER

Inadvertent adjustment of the parameters

Risk of death due to failure of the safety function!

- ▶ Secure the device against unintentional adjustment.

The front-end DIP switches can be used to set the direction of action of the switching output for each channel separately and to activate input circuit monitoring for wire break and short circuit.

Toggle mode	Meaning
NO	operating current
NC	Quiescent current behavior
WB	Wire-break monitoring activated
SC	Short-circuit monitoring activated
LM	Input circuit monitoring for wire break and short circuit (MK13-R-Ex0 only)
off	The function in question is deactivated



Fig. 10: Adjustments via DIP switch

The following function table lists the various input states with the associated output states. It should be noted that the switching behavior of inductive sensors in accordance with EN 60947-5-6 (NAMUR) generally corresponds to that of mechanical NC contacts. The switching behavior of capacitive and magnetic-inductive sensors corresponds to that of NO contacts.

Wirkungsrichtung Function mode Sens d'action	Eingang/input/entrée		Ausgang/output/sortie			
	Induktiver Sensor inductive sensor détecteur inductif EN 60947-5-6 NAMUR	mechanischer Kontakt dry contact contact mécanique R1 = 1...2,2 kΩ (> ¼ W) R2 = 10...22 kΩ (> ¼ W)	kein Fehler/normal/sans défaut	IM1-121Ex-... Störmeldeausgang alarm output sortie de sig. de défaut	mit Fehler/short or wire-break/avec défaut	IM1-121Ex-... Störmeldeausgang alarm output sortie de sig. de défaut
			Schaltausgang switching output sortie de commutation		Schaltausgang switching output sortie de commutation	
Arbeitsstromverhalten load current mode (N.O.) fonction travail NO			0	1	0	0
			1	1	0	0
Ruhestromverhalten no load current mode (N.C.) fonction repos NC			1	1	0	0
			0	1	0	0

Fig. 11: Function table

6 Operation, maintenance and repair

The specifications apply to the operating conditions in an industrial environment according to IEC 606541-1 Class C (protected location) with an ambient temperature of 40 °C over a long period of time.

6.1 Troubleshooting

The correction of faults is described in the instructions for use of the respective device.



NOTE

The user must immediately report to Turck any faults on the device that occur when the device is used in safety-relevant applications.

6.2 Maintenance

Ensure that the plug connections and cables are always in good condition.
The devices are maintenance-free; clean using dry materials as required.



DANGER

Malfunction due to conductive media or static charge

Risk of death due to failure of the safety function!

- ▶ Do not use liquid media or static cleaning agents when cleaning.



DANGER

Inadvertent adjustment of the parameters

Risk of death due to failure of the safety function!

- ▶ Perform a functional test after each cleaning.

6.3 Repair



DANGER

The device must not be repaired.

Risk of death due to malfunction!

- ▶ Send the device to Turck for repair. Please observe the specific warranty conditions agreed with the delivery.

6.3.1 Returning devices

If a device has to be returned, bear in mind that only devices with a decontamination declaration will be accepted. This is available for download at www.turck.de/de/produkt-retoure-6079.php and must be completely filled in, and affixed securely and weather-proof to the outside of the packaging.

7 Decommissioning and retirement

7.1 Decommissioning

The decommissioning procedure is described in the operating instructions for the respective device.

7.2 Retirement



The devices must be retired after their useful lifetime of 8...12 years has expired. The devices must be disposed of properly and do not belong in the domestic waste.

8 Appendix — EXIDA-Report FMEDA Turck 04/07-14 R002



Failure Modes, Effects and Diagnostic Analysis

Project:

Isolating Switching Amplifiers IM1-**(Ex)-* and MK13-R-Ex0

Customer:

Hans Turck GmbH & Co. KG
Mühlheim
Germany

Contract No.: TURCK 04/07-14

Report No.: TURCK 04/07-14 R002

Version V3, Revision R0, February 2014

Stephan Aschenbrenner

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Management summary

This report summarizes the results of the hardware assessment carried out on the Isolating Switching Amplifiers IM1-**(Ex)-* and MK13-R-Ex0.

Table 1 gives an overview of the different versions that belong to the considered devices.

The hardware assessment consists of a Failure Modes, Effects and Diagnostics Analysis (FMEDA). A FMEDA is one of the steps taken to achieve functional safety assessment of a device per IEC 61508. From the FMEDA, failure rates are determined and consequently the Safe Failure Fraction (SFF) is calculated for the device. For full assessment purposes all requirements of IEC 61508 must be considered.

Table 1: Version overview

Type	Description ¹	Parts List / Circuit Diagram
IM1-12Ex-R IM1-12-R	1 input / 2 relay outputs	12296307 of 07.10.04 / 12296307 of 28.09.04
IM1-12Ex-T IM1-12-T	1 input / 2 transistor outputs	12296309 of 07.10.04 / 12296309 of 28.09.04
IM1-22Ex-R IM1-22-R	2 inputs / 2 relay outputs	12296301 of 07.10.04 / 12296301 of 28.09.04
IM1-22Ex-T IM1-22-T	2 inputs / 2 transistor outputs	12296303 of 13.08.04 / 12296303 of 28.09.04
IM1-121Ex-R	1 input / 2 relay outputs (one used as error message output)	12296310 of 07.10.04 / 12296310 of 28.09.04
IM1-121Ex-T	1 input / 2 transistor outputs (one used as error message output)	12296312 of 25.01.05 / 12296312 of 28.09.04
MK13-R-Ex0	1 input / 1 relay output	12296101 of 18.10.04 / 12296100 of 07.10.04

The failure rates used in this analysis are the basic failure rates from the Siemens standard SN 29500.

According to table 2 of IEC 61508-1 the average PFD for systems operating in low demand mode has to be $\geq 10^{-3}$ to $< 10^{-2}$ for SIL 2 safety functions. However, as the modules under consideration are only one part of an entire safety function they should not claim more than 10% of this range, i.e. they should be better than or equal to 1,00E-03.

The Isolating Switching Amplifiers IM1-**(Ex)-* and MK13-R-Ex0 are considered to be Type A² components with a hardware fault tolerance of 0.

For Type A components the SFF has to be 60% to $< 90\%$ according to table 2 of IEC 61508-2 for SIL 2 (sub-) systems with a hardware fault tolerance of 0.

The following failure rates are valid for operating stress conditions typical of an industrial field environment similar to IEC 60654-1 class C (sheltered location) with an average temperature over a long period of time of 40°C. For a higher average temperature of 60°C, the failure rates should be multiplied with an experience based factor of 2,5. A similar multiplier should be used if frequent temperature fluctuation must be assumed.

¹ The two channels on a redundant board shall not be used to increase the hardware fault tolerance needed for a higher SIL as they contain common components.

² Type A component: "Non-complex" component (all failure modes are well defined); for details see 7.4.3.1.2 of IEC 61508-2.



Table 2: Summary for MK13-R-Ex0 – Failure rates

λ_{safe}	$\lambda_{\text{dangerous}}$	SFF
288 FIT	110 FIT	72%

Table 3: Summary for MK13-R-Ex0 – PFD_{AVG} values

T[Proof] = 1 year	T[Proof] = 5 years	T[Proof] = 10 years
PFD _{AVG} = 4,80E-04	PFD _{AVG} = 2,40E-03	PFD _{AVG} = 4,79E-03

Table 4: Summary for IM1-*-R – Failure rates**

λ_{safe}	$\lambda_{\text{dangerous}}$	SFF
299 FIT	110 FIT	73%

Table 5: Summary for IM1-*-R – PFD_{AVG} values**

T[Proof] = 1 year	T[Proof] = 5 years	T[Proof] = 10 years
PFD _{AVG} = 4,80E-04	PFD _{AVG} = 2,40E-03	PFD _{AVG} = 4,79E-03

Table 6: Summary for IM1-*-T – Failure rates**

λ_{safe}	$\lambda_{\text{dangerous}}$	SFF
267 FIT	85 FIT	75%

Table 7: Summary for IM1-*-T – PFD_{AVG} values**

T[Proof] = 1 year	T[Proof] = 5 years	T[Proof] = 10 years
PFD _{AVG} = 3,72E-04	PFD _{AVG} = 1,86E-03	PFD _{AVG} = 3,71E-03

The boxes marked in yellow () mean that the calculated PFD_{AVG} values are within the allowed range for SIL 2 according to table 2 of IEC 61508-1 but do not fulfill the requirement to not claim more than 10% of this range, i.e. to be better than or equal to 1,00E-03. The boxes marked in green () mean that the calculated PFD_{AVG} values are within the allowed range for SIL 2 according to table 2 of IEC 61508-1 and table 3.1 of ANSI/ISA–84.01–1996 and do fulfill the requirement to not claim more than 10% of this range, i.e. to be better than or equal to 1,00E-03.

Because the Safe Failure Fraction (SFF) is above 60%, also the architectural constraints requirements of table 2 of IEC 61508-2 for Type A subsystems with a Hardware Fault Tolerance (HFT) of 0 are fulfilled.

A user of the Isolating Switching Amplifiers IM1-**(Ex)-* and MK13-R-Ex0 can utilize these failure rates in a probabilistic model of a safety instrumented function (SIF) to determine suitability in part for safety instrumented system (SIS) usage in a particular safety integrity level (SIL). A full table of failure rates is presented in sections 5.1 to 5.3 along with all assumptions.

The failure rates are valid for the useful life of the Isolating Switching Amplifiers IM1-**(Ex)-* and MK13-R-Ex0, which is estimated to be between 8 and 12 years (see Appendix 2).

It is important to realize that the “no effect” failures are included in the “safe undetected” failure category according to IEC 61508. Note that these failures on its own will not affect system reliability or safety, and should not be included in spurious trip calculations.



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1 Purpose and Scope

Generally three options exist when doing an assessment of sensors, interfaces and/or final elements.

Option 1: Hardware assessment according to IEC 61508

Option 1 is a hardware assessment by *exida.com* according to the relevant functional safety standard(s) like DIN V VDE 0801, IEC 61508 or EN 954-1. The hardware assessment consists of a FMEDA to determine the fault behavior and the failure rates of the device, which are then used to calculate the Safe Failure Fraction (SFF) and the average Probability of Failure on Demand (PFD_{AVG}).

This option for pre-existing hardware devices shall provide the safety instrumentation engineer with the required failure data as per IEC 61508 / IEC 61511 and does not include an assessment of the software development process

Option 2: Hardware assessment with proven-in-use consideration according to IEC 61508 / IEC 61511

Option 2 is an assessment by *exida.com* according to the relevant functional safety standard(s) like DIN V VDE 0801, IEC 61508 or EN 954-1. The hardware assessment consists of a FMEDA to determine the fault behavior and the failure rates of the device, which are then used to calculate the Safe Failure Fraction (SFF) and the average Probability of Failure on Demand (PFD_{AVG}). In addition this option consists of an assessment of the proven-in-use documentation of the device and its software including the modification process.

This option for pre-existing programmable electronic devices shall provide the safety instrumentation engineer with the required failure data as per IEC 61508 / IEC 61511 and justify the reduced fault tolerance requirements of IEC 61511 for sensors, final elements and other PE field devices.

Option 3: Full assessment according to IEC 61508

Option 3 is a full assessment by *exida.com* according to the relevant application standard(s) like IEC 61511 or EN 298 and the necessary functional safety standard(s) like DIN V VDE 0801, IEC 61508 or EN 954-1. The full assessment extends option 1 by an assessment of all fault avoidance and fault control measures during hardware and software development.

This option is most suitable for newly developed software based field devices and programmable controllers to demonstrate full compliance with IEC 61508 to the end-user.

This assessment shall be done according to option 1.

This document shall describe the results of the hardware assessment carried out on the Isolating Switching Amplifiers IM1-**(Ex)-* and MK13-R-Ex0.

It shall be assessed whether the described devices meet the average Probability of Failure on Demand (PFD_{AVG}) requirements and the architectural constraints for SIL 2 sub-systems according to IEC 61508.

It **does not** consider any calculations necessary for proving intrinsic safety.



2 Project management

2.1 exida.com

exida.com is one of the world's leading knowledge companies specializing in automation system safety and availability with over 100 years of cumulative experience in functional safety. Founded by several of the world's top reliability and safety experts from assessment organizations like TUV and manufacturers, *exida.com* is a partnership with offices around the world. *exida.com* offers training, coaching, project oriented consulting services, internet based safety engineering tools, detail product assurance and certification analysis and a collection of on-line safety and reliability resources. *exida.com* maintains a comprehensive failure rate and failure mode database on process equipment.

2.2 Roles of the parties involved

Werner Turck GmbH & Co. KG Manufacturer of the considered Isolating Switching Amplifiers IM1-**(Ex)-* and MK13-R-Ex0.
exida.com Performed the hardware assessment according to option 1 (see section 1).

Werner Turck GmbH & Co. KG contracted *exida.com* in August 2004 with the FMEDA and PFD_{AVG} calculation of the above mentioned device.

2.3 Standards / Literature used

The services delivered by *exida.com* were performed based on the following standards / literature.

[N1]	IEC 61508-2:2000	Functional Safety of Electrical/Electronic/Programmable Electronic Safety-Related Systems
[N2]	ISBN: 0471133019 John Wiley & Sons	Electronic Components: Selection and Application Guidelines by Victor Meeldijk
[N3]	FMD-91, RAC 1991	Failure Mode / Mechanism Distributions
[N4]	FMD-97, RAC 1997	Failure Mode / Mechanism Distributions
[N5]	NPRD-95, RAC	Non-electronic Parts – Reliability Data 1995
[N6]	SN 29500	Failure rates of components

2.4 Reference documents

2.4.1 Documentation provided by the customer

[D1]	im1_22Ex0_R.pdf	Description of the working principle
[D2]	im1_22Ex0_T.pdf	Description of the working principle
[D3]	D201010.pdf	Data sheet Isolating switching amplifier IM1-12Ex-R 1-channel
[D4]	D201006.pdf	Data sheet Isolating switching amplifier IM1-12Ex-T 1-channel
[D5]	D201014.pdf	Data sheet Isolating switching amplifier IM1-22Ex-R 2-channel



[D6]	D201015.pdf	Data sheet Isolating switching amplifier IM1-22Ex-T 2-channel
[D7]	D201021.pdf	Data sheet Isolating switching amplifier IM1-121Ex-R 1-channel
[D8]	d201030.pdf	Data sheet Isolating switching amplifier IM1-121Ex-T 1-channel
[D9]	MK13_R_Ex0SL.pdf	Parts list 12296101 of 18.10.04
[D10]	MK13_R_Ex0Sch.pdf	Circuit diagram 12296100 of 07.10.04
[D11]	IM1_12ExRSL.pdf	Parts list 12296307 of 07.10.04
[D12]	IM1_12ExRSch.pdf	Circuit diagram 12296307 of 28.09.04
[D13]	IM1_12ExTSL.pdf	Parts list 12296309 of 07.10.04
[D14]	IM1_12ExTSch.pdf	Circuit diagram 12296309 of 28.09.04
[D15]	IM1_22ExRSL.pdf	Parts list 12296301 of 07.10.04
[D16]	IM1_22ExRSch.pdf	Circuit diagram 12296301 of 28.09.04
[D17]	IM1_22ExTSL.pdf	Parts list 12296303 of 13.08.04
[D18]	IM1_22ExTSch.pdf	Circuit diagram 12296303 of 28.09.04
[D19]	IM1_121Ex_R.pdf	Parts list 12296310 of 07.10.04
[D20]	IM1_121_ExRSch.pdf	Circuit diagram 12296310 of 28.09.04
[D21]	IM1_121Ex_T.pdf	Parts list 12296312 of 25.01.05
[D22]	IM1_121_TSch.pdf	Circuit diagram 12296312 of 28.09.04
[D23]	Manual.pdf	Manual of the ASIC
[D24]	SchaltungASIC.pdf	Circuit diagram of the ASIC
[D25]	LayoutASIC.pdf	Layout of the ASIC

2.4.2 Documentation generated by *exida.com*

[R1]	FMEDA V6 MK13-R-Ex0 V1 R1.0.xls of 11.03.05
[R2]	FMEDA V6 IM1-12Ex-R V1 R1.0.xls of 11.03.05
[R3]	FMEDA V6 IM1-12Ex-T V1 R1.0.xls of 11.03.05
[R4]	FMEDA V6 ASIC 5V regulator V0 R1.0.xls of 08.03.05
[R5]	FMEDA V6 ASIC 8V regulator V0 R1.0.xls of 07.03.05
[R6]	FMEDA V6 ASIC error signal path V0 R1.0.xls of 08.03.05
[R7]	FMEDA V6 ASIC NAMUR signal path detailed V0 R1.0.xls of 08.03.05
[R8]	FMEDA V6 ASIC PU block V0 R1.0.xls of 07.03.05
[R9]	FMEDA V6 ASIC remaining parts V0 R1.0.xls of 08.03.05
[R10]	FMEDA V6 ASIC partly detailed V0 R1.0.xls of 08.03.05
[R11]	Besprechung ASIC 07.03.05.txt

3 Description of the analyzed modules

The Isolating Switching Amplifiers IM1-**(Ex)-* and MK13-R-Ex0 consist of intrinsically safe input circuits.

They can be connected to sensors according to EN 60947-5-6 (NAMUR), variable resistors or potential-free contacts.

The output circuits, galvanically isolated from the input circuits, consist of either relay outputs or transistor outputs.

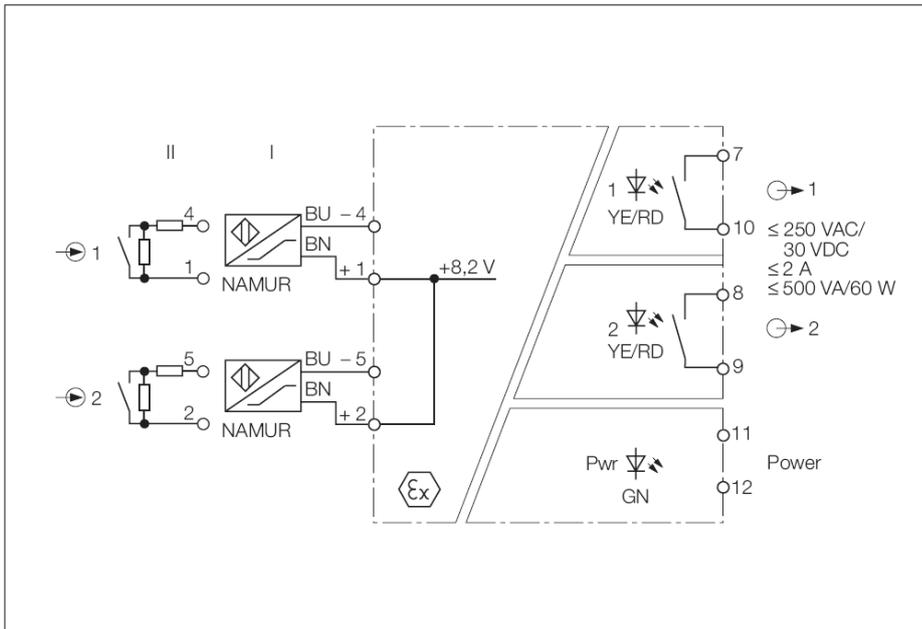


Figure 1: Block diagram of the Isolating Switching Amplifier IM1-22Ex-R

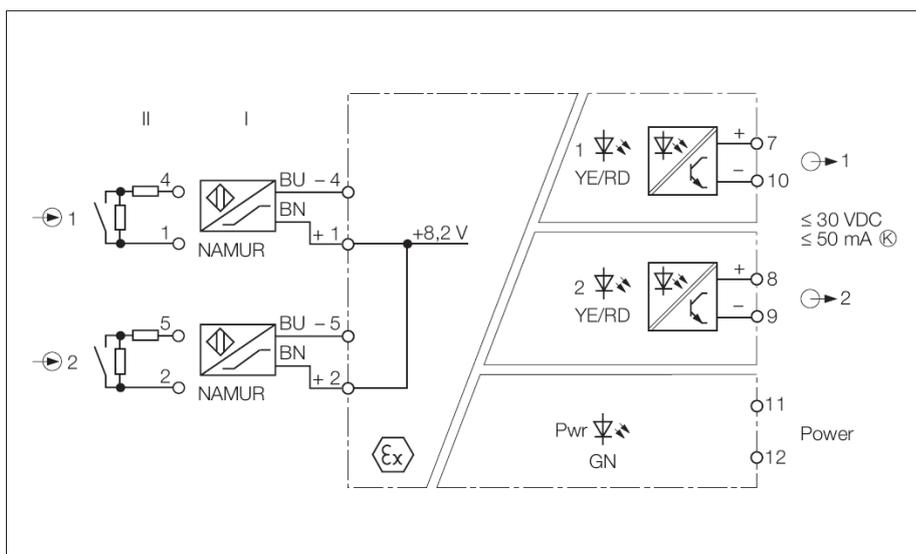


Figure 2: Block diagram of the Isolating Switching Amplifier IM1-22Ex-T



The block diagrams above show the working principal of all considered versions with the exception that the presented block diagrams have two input and two output channels. The differences between the versions are described in Table 1.

The Isolating Switching Amplifiers IM1-**(Ex)-* and MK13-R-Ex0 are considered to be Type A components with a hardware fault tolerance of 0.

Although the Isolating Switching Amplifiers IM1-**(Ex)-* and MK13-R-Ex0 are designed with a semi-custom ASIC 724 from ZETEX (see [D23]) they are still considered to be Type A components. The reason is the low complexity, the full analyzability of the used ASIC and the fact that the ASIC does not contain hidden state information such as internal digital registers (see [D24]). It only consists of 103 transistors, 908 resistors and 7 junction capacitors, which can individually be connected (see [D25]).

exida.com did a detailed analysis of the ASIC based on the individual failure modes of the internal transistors, resistors and capacitors (see [R4] to [R11]). Possible dependencies were taken into account with a common cause factor of 25%. The failure rate from the Siemens standard SN 29500 for a bipolar ECL ASIC with 50 to 5000 transistors was multiplied with a safety factor of 2. The resulting 100 FIT were used in the overall analysis for the Isolating Switching Amplifiers IM1-**(Ex)-* and MK13-R-Ex0.



4 Failure Modes, Effects, and Diagnostic Analysis

The Failure Modes, Effects, and Diagnostic Analysis was done together with Werner Turck GmbH & Co. KG and is documented in [R2] to [R10]. Failures can be classified according to the following failure categories.

4.1 Description of the failure categories

In order to judge the failure behavior of the Isolating Switching Amplifiers IM1-**(Ex)-* and MK13-R-Ex0, the following definitions for the failure of the product were considered.

Fail-Safe State	The fail-safe state is defined as the output being de-energized. This corresponds to an input signal of less than 1.4mA (NAMUR signal).
Fail Safe	Failure that causes the module / (sub)system to go to the defined fail-safe state without a demand from the process.
Fail Dangerous	Failure that does not respond to a demand from the process (i.e. being unable to go to the defined fail-safe state).
No Effect	Failure of a component that is part of the safety function but that has no effect on the safety function. For the calculation of the SFF it is treated like a safe undetected failure.
Not part	Failures of a component which is not part of the safety function but part of the circuit diagram and is listed for completeness. When calculating the SFF this failure mode is not taken into account. It is also not part of the total failure rate.

The “no effect” failures are provided for those who wish to do reliability modeling more detailed than required by IEC 61508. In IEC 61508 the “no effect” failures are defined as safe undetected failures even though they will not cause the safety function to go to a safe state. Therefore they need to be considered in the Safe Failure Fraction calculation.

4.2 Methodology – FMEDA, Failure rates

4.2.1 FMEDA

A Failure Modes and Effects Analysis (FMEA) is a systematic way to identify and evaluate the effects of different component failure modes, to determine what could eliminate or reduce the chance of failure, and to document the system in consideration.

A FMEDA (Failure Modes, Effects, and Diagnostic Analysis) is a FMEA extension. It combines standard FMEA techniques with extension to identify online diagnostics techniques and the failure modes relevant to safety instrumented system design. It is a technique recommended to generate failure rates for each important category (safe detected, safe undetected, dangerous detected, dangerous undetected, fail high, fail low) in the safety models. The format for the FMEDA is an extension of the standard FMEA format from MIL STD 1629A, Failure Modes and Effects Analysis.



4.2.2 Failure rates

The failure rate data used by *exida.com* in this FMEDA are the basic failure rates from the Siemens SN 29500 failure rate database. The rates are considered to be appropriate for safety integrity level verification calculations. The rates match operating stress conditions typical of an industrial field environment similar to IEC 60654-1, class C. It is expected that the actual number of field failures will be less than the number predicted by these failure rates.

The user of these numbers is responsible for determining their applicability to any particular environment. Accurate plant specific data may be used for this purpose. If a user has data collected from a good proof test reporting system that indicates higher failure rates, the higher numbers shall be used. Some industrial plant sites have high levels of stress. Under those conditions the failure rate data is adjusted to a higher value to account for the specific conditions of the plant.

4.2.3 Assumptions

The following assumptions have been made during the Failure Modes, Effects, and Diagnostic Analysis of the Isolating Switching Amplifiers IM1-**(Ex)-* and MK13-R-Ex0.

- Failure rates are constant, wear out mechanisms are not included.
- Propagation of failures is not relevant.
- The time to restoration after a safe failure is 8 hours.
- All modules are operated in the low demand mode of operation.
- External power supply failure rates are not included.
- Only one input and one output are part of the safety function
- Sufficient tests are performed prior to shipment to verify the absence of vendor and/or manufacturing defects that prevent proper operation of specified functionality to product specifications or cause operation different from the design analyzed.
- The two channels on a redundant board are not used to increase the hardware fault tolerance needed for a higher SIL as they contain common components.
- The stress levels are average for an industrial environment and can be compared to the Ground Fixed classification of MIL-HNBK-217F. Alternatively, the assumed environment is similar to:
 - IEC 60654-1, Class C (sheltered location) with temperature limits within the manufacturer's rating and an average temperature over a long period of time of 40°C. Humidity levels are assumed within manufacturer's rating.

5 Results of the assessment

exida.com did the FMEDAs together with Werner Turck GmbH & Co. KG.

For the calculation of the Safe Failure Fraction (SFF) the following has to be noted:

λ_{total} consists of the sum of all component failure rates. This means:

$$\lambda_{total} = \lambda_{safe} + \lambda_{dangerous} + \lambda_{no\ effect}$$

$$SFF = 1 - \lambda_{du} / \lambda_{total}$$

For the FMEDAs failure modes and distributions were used based on information gained from [N3] to [N5].

For the calculation of the PFD_{AVG} the following Markov model for 1oo1 system was used. As after a complete proof test all states are going back to the OK state no proof test rate is shown in the Markov models but included in the calculation.

The proof test time was changed using the Microsoft® Excel 2000 based FMEDA tool of *exida.com* as a simulation tool. The results are documented in the following sections.

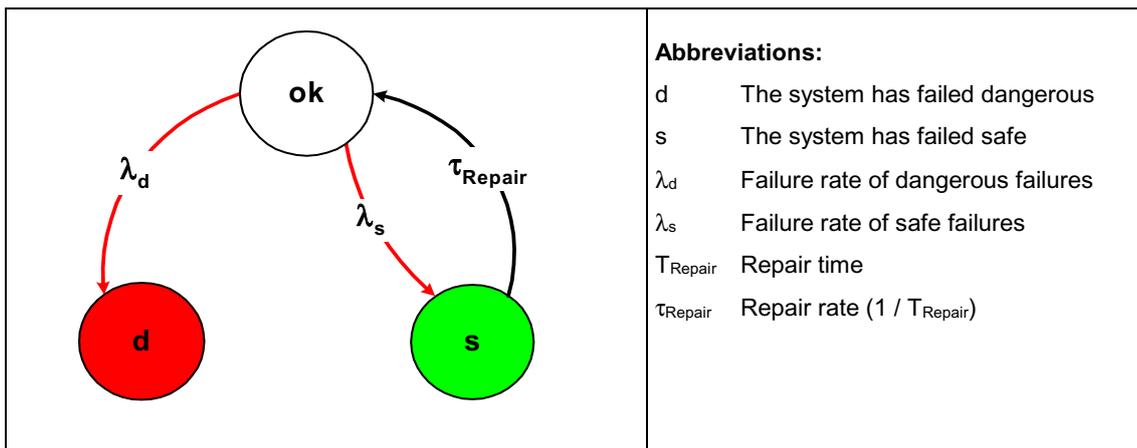


Figure 3: Markov model for a 1oo1 structure



5.1 Isolating Switching Amplifier MK13-R-Ex0

The FMEDA carried out on the Isolating Switching Amplifier MK13-R-Ex0 leads under the assumptions described in sections 4.2.3 and 5 to the following failure rates:

$$\lambda_{sd} = 0,00E-00 \text{ 1/h}$$

$$\lambda_{su} = 1,66E-07 \text{ 1/h}$$

$$\lambda_{dd} = 0,00E-00 \text{ 1/h}$$

$$\lambda_{du} = 1,10E-07 \text{ 1/h}$$

$$\lambda_{no \text{ effect}} = 1,22E-07 \text{ 1/h}$$

$$\lambda_{total} = 3,98E-07 \text{ 1/h}$$

$$\lambda_{not \text{ part}} = 1,04E-08 \text{ 1/h}$$

$$MTBF = MTTF + MTTR = 1 / (\lambda_{total} + \lambda_{not \text{ part}}) + 8 \text{ h} = 279 \text{ years}$$

Under the assumptions described in section 5 and the definitions given in section 4.1 the following table shows the failure rates according to IEC 61508:

λ_{safe}	$\lambda_{dangerous}$	SFF
288 FIT	110 FIT	72,44%

The PFD_{AVG} was calculated for three different proof test times using the Markov model as described in Figure 3.

T[Proof] = 1 year	T[Proof] = 5 years	T[Proof] = 10 years
PFD _{AVG} = 4,80E-04	PFD _{AVG} = 2,40E-03	PFD _{AVG} = 4,79E-03

The boxes marked in yellow () mean that the calculated PFD_{AVG} values are within the allowed range for SIL 2 according to table 2 of IEC 61508-1 and table 3.1 of ANSI/ISA-84.01-1996 but do not fulfill the requirement to not claim more than 10% of this range, i.e. to be better than or equal to 1,00E-03. The boxes marked in green () mean that the calculated PFD_{AVG} values are within the allowed range for SIL 2 according to table 2 of IEC 61508-1 and table 3.1 of ANSI/ISA-84.01-1996 and do fulfill the requirement to not claim more than 10% of this range, i.e. to be better than or equal to 1,00E-03. Figure 4 shows the time dependent curve of PFD_{AVG}.

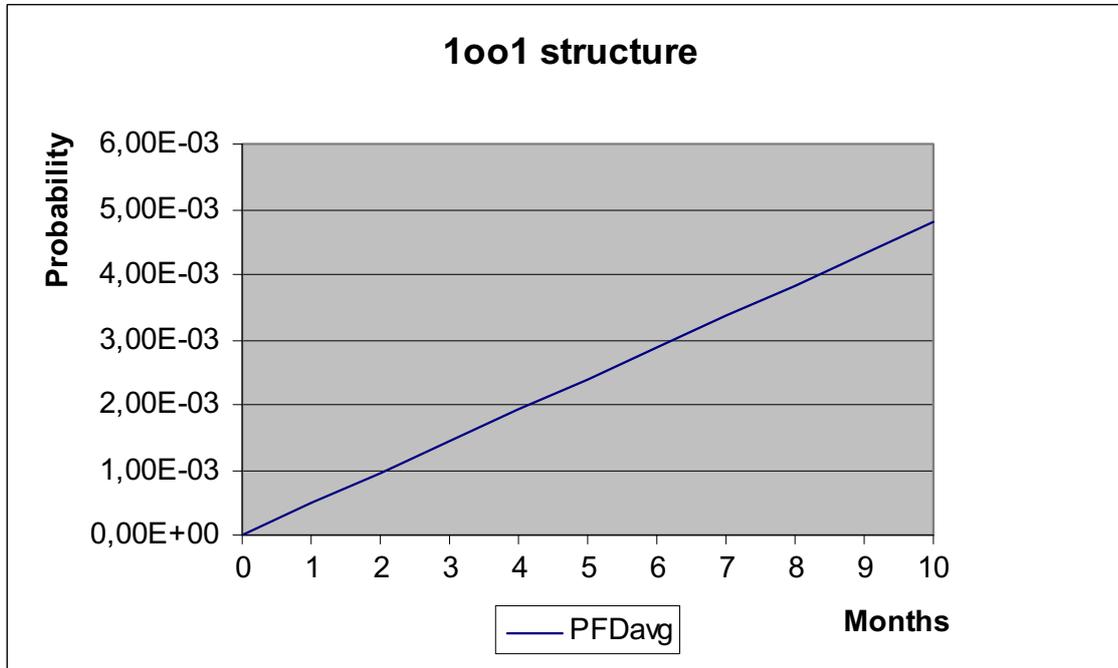


Figure 4: PFD_{AVG}(t)



5.2 Isolating Switching Amplifier IM1-***-R

The FMEDA carried out on the Isolating Switching Amplifier IM1-***-R leads under the assumptions described in sections 4.2.3 and 5 to the following failure rates:

$$\lambda_{sd} = 0,00E-00 \text{ 1/h}$$

$$\lambda_{su} = 1,72E-07 \text{ 1/h}$$

$$\lambda_{dd} = 0,00E-00 \text{ 1/h}$$

$$\lambda_{du} = 1,10E-07 \text{ 1/h}$$

$$\lambda_{no \text{ effect}} = 1,27E-07 \text{ 1/h}$$

$$\lambda_{total} = 4,09E-07 \text{ 1/h}$$

$$\lambda_{not \text{ part}} = 1,10E-08 \text{ 1/h}$$

$$MTBF = MTTF + MTTR = 1 / (\lambda_{total} + \lambda_{not \text{ part}}) + 8 \text{ h} = 272 \text{ years}$$

Under the assumptions described in section 5 and the definitions given in section 4.1 the following table shows the failure rates according to IEC 61508:

λ_{safe}	$\lambda_{dangerous}$	SFF
299 FIT	110 FIT	73,15%

The PFD_{AVG} was calculated for three different proof test times using the Markov model as described in Figure 3.

T[Proof] = 1 year	T[Proof] = 5 years	T[Proof] = 10 years
$PFD_{AVG} = 4,80E-04$	$PFD_{AVG} = 2,40E-03$	$PFD_{AVG} = 4,79E-03$

The boxes marked in yellow () mean that the calculated PFD_{AVG} values are within the allowed range for SIL 2 according to table 2 of IEC 61508-1 and table 3.1 of ANSI/ISA-84.01-1996 but do not fulfill the requirement to not claim more than 10% of this range, i.e. to be better than or equal to $1,00E-03$. The boxes marked in green () mean that the calculated PFD_{AVG} values are within the allowed range for SIL 2 according to table 2 of IEC 61508-1 and table 3.1 of ANSI/ISA-84.01-1996 and do fulfill the requirement to not claim more than 10% of this range, i.e. to be better than or equal to $1,00E-03$. Figure 5 shows the time dependent curve of PFD_{AVG} .

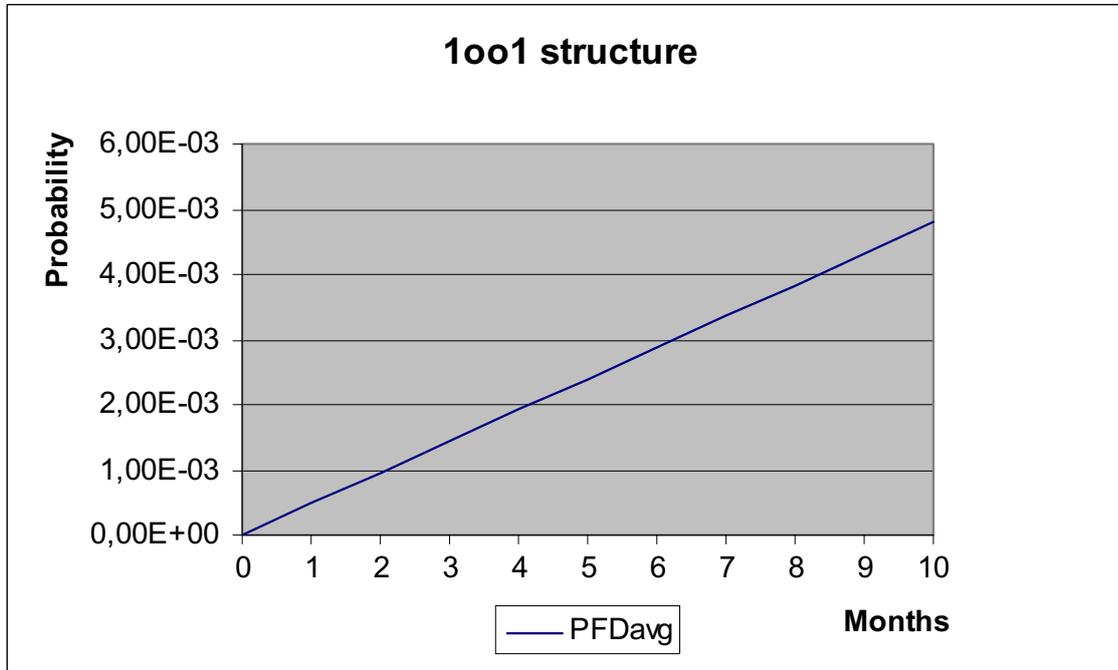


Figure 5: PFD_{AVG}(t)



5.3 Isolating Switching Amplifier IM1-***-T

The FMEDA carried out on the Isolating Switching Amplifier IM1-***-T leads under the assumptions described in sections 4.2.3 and 5 to the following failure rates:

$$\lambda_{sd} = 0,00E-00 \text{ 1/h}$$

$$\lambda_{su} = 1,44E-07 \text{ 1/h}$$

$$\lambda_{dd} = 0,00E-00 \text{ 1/h}$$

$$\lambda_{du} = 8,49E-08 \text{ 1/h}$$

$$\lambda_{no \text{ effect}} = 1,23E-07 \text{ 1/h}$$

$$\lambda_{total} = 3,52E-07 \text{ 1/h}$$

$$\lambda_{not \text{ part}} = 1,10E-08 \text{ 1/h}$$

$$MTBF = MTTF + MTTR = 1 / (\lambda_{total} + \lambda_{not \text{ part}}) + 8 \text{ h} = 314 \text{ years}$$

Under the assumptions described in section 5 and the definitions given in section 4.1 the following table shows the failure rates according to IEC 61508:

λ_{safe}	$\lambda_{dangerous}$	SFF
267 FIT	85 FIT	75,89%

The PFD_{AVG} was calculated for three different proof test times using the Markov model as described in Figure 3.

T[Proof] = 1 year	T[Proof] = 5 years	T[Proof] = 10 years
PFD _{AVG} = 3,72E-04	PFD _{AVG} = 1,86E-03	PFD _{AVG} = 3,71E-03

The boxes marked in yellow () mean that the calculated PFD_{AVG} values are within the allowed range for SIL 2 according to table 2 of IEC 61508-1 and table 3.1 of ANSI/ISA-84.01-1996 but do not fulfill the requirement to not claim more than 10% of this range, i.e. to be better than or equal to 1,00E-03. The boxes marked in green () mean that the calculated PFD_{AVG} values are within the allowed range for SIL 2 according to table 2 of IEC 61508-1 and table 3.1 of ANSI/ISA-84.01-1996 and do fulfill the requirement to not claim more than 10% of this range, i.e. to be better than or equal to 1,00E-03. Figure 6 shows the time dependent curve of PFD_{AVG}.

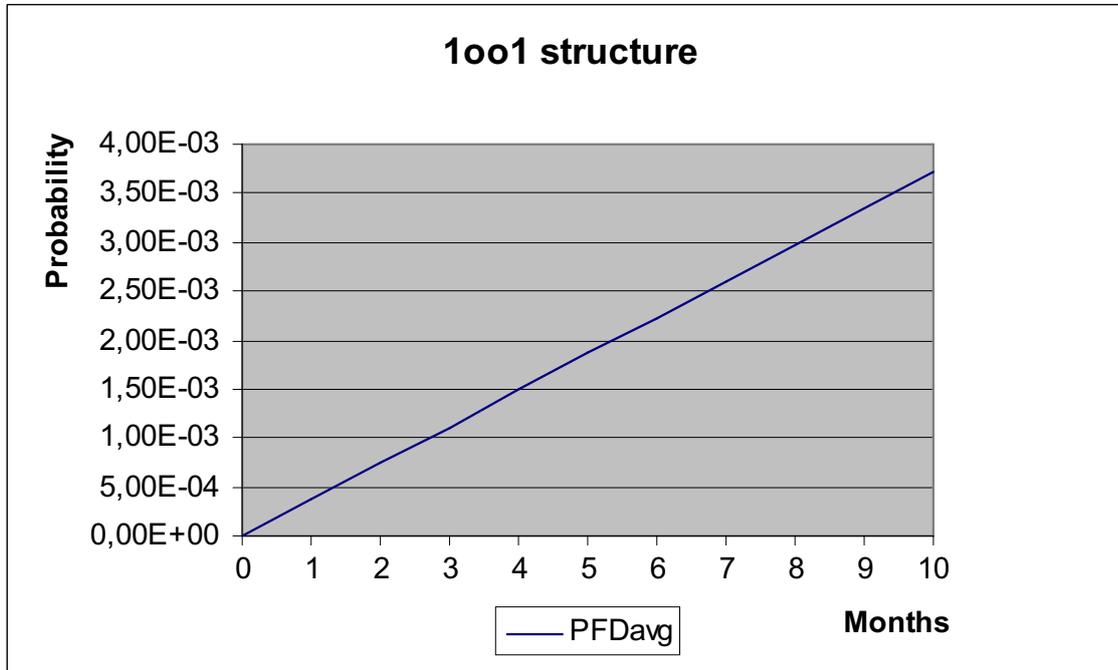


Figure 6: PFD_{AVG}(t)



6 Terms and Definitions

FIT	Failure In Time (1×10^{-9} failures per hour)
FMEDA	Failure Modes, Effects, and Diagnostic Analysis
HFT	Hardware Fault Tolerance
Low demand mode	Mode, where the frequency of demands for operation made on a safety-related system is no greater than one per year and no greater than twice the proof test frequency.
PFD_{AVG}	Average Probability of Failure on Demand
SFF	Safe Failure Fraction summarizes the fraction of failures, which lead to a safe state and the fraction of failures which will be detected by diagnostic measures and lead to a defined safety action.
SIF	Safety Instrumented Function
SIL	Safety Integrity Level
Type A component	“Non-complex” component (all failure modes are well defined); for details see 7.4.3.1.2 of IEC 61508-2.
T[Proof]	Proof Test Interval



7 Status of the document

7.1 Liability

exida prepares reports based on methods advocated in International standards. Failure rates are obtained from a collection of industrial databases. *exida* accepts no liability whatsoever for the use of these numbers or for the correctness of the standards on which the general calculation methods are based.

Due to future potential changes in the standards, best available information and best practices, the current FMEDA results presented in this report may not be fully consistent with results that would be presented for the identical product at some future time. As a leader in the functional safety market place, *exida* is actively involved in evolving best practices prior to official release of updated standards so that our reports effectively anticipate any known changes. In addition, most changes are anticipated to be incremental in nature and results reported within the previous three year period should be sufficient for current usage without significant question.

Most products also tend to undergo incremental changes over time. If an *exida* FMEDA has not been updated within the last three years and the exact results are critical to the SIL verification you may wish to contact the product vendor to verify the current validity of the results.

7.2 Releases

Version History: V3R0: IM1-12-R, IM1-12-T and IM1-22-T added; February 21, 2014
V2R0: IM1-22-R added; February 8, 2013
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Authors: Stephan Aschenbrenner

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7.3 Release Signatures

A handwritten signature in black ink, appearing to be 'S. Aschenbrenner', written over a horizontal line.

Dipl.-Ing. (Univ.) Stephan Aschenbrenner, Partner

A handwritten signature in black ink, appearing to be 'R. Faller', written over a horizontal line.

Dipl.-Ing. (Univ.) Rainer Faller, Principal Partner



Appendix 1: Possibilities to reveal dangerous undetected faults during the proof test

According to section 7.4.3.2.2 f) of IEC 61508-2 proof tests shall be undertaken to reveal dangerous faults which are undetected by diagnostic tests.

This means that it is necessary to specify how dangerous undetected faults which have been noted during the FMEDA can be detected during proof testing.

Table 8, Table 9 and Table 10 show an importance analysis of the most critical dangerous undetected faults and indicate how these faults can be detected during proof testing.

Appendix 1 shall be considered when writing the safety manual as it contains important safety related information.

Table 8: Importance Analysis of dangerous undetected faults of MK13-R-Ex0

Component	% of total λ_{du}	Detection through
IC3	60,90%	100% functional test with monitoring of the expected output signal
K1	22,78%	100% functional test with monitoring of the expected output signal
T101	10,03%	100% functional test with monitoring of the expected output signal
IC1	4,10%	100% functional test with monitoring of the expected output signal
D101	0,91%	100% functional test with monitoring of the expected output signal
C101	0,91%	100% functional test with monitoring of the expected output signal
X4	0,18%	100% functional test with monitoring of the expected output signal
R101	0,18%	100% functional test with monitoring of the expected output signal

Table 9: Importance Analysis of dangerous undetected faults of IM1-*-R**

Component	% of total λ_{du}	Detection through
IC4	60,90%	100% functional test with monitoring of the expected output signal
K1	22,78%	100% functional test with monitoring of the expected output signal
T102	10,03%	100% functional test with monitoring of the expected output signal
IC1	4,10%	100% functional test with monitoring of the expected output signal
D100	0,91%	100% functional test with monitoring of the expected output signal
C100	0,91%	100% functional test with monitoring of the expected output signal
X1	0,18%	100% functional test with monitoring of the expected output signal
R100	0,18%	100% functional test with monitoring of the expected output signal



Table 10: Importance Analysis of dangerous undetected faults of IM1-*-T**

Component	% of total λ_{du}	Detection through
IC4	78,73%	100% functional test with monitoring of the expected output signal
T202	12,96%	100% functional test with monitoring of the expected output signal
IC2	5,30%	100% functional test with monitoring of the expected output signal
D100	1,18%	100% functional test with monitoring of the expected output signal
C100	1,18%	100% functional test with monitoring of the expected output signal
X1	0,24%	100% functional test with monitoring of the expected output signal
R100	0,24%	100% functional test with monitoring of the expected output signal
D203	0,18%	100% functional test with monitoring of the expected output signal



Appendix 1.1: Possible proof tests to detect dangerous undetected faults

The proof test consists of the following steps, as described in Table 11.

Table 11 Steps for Proof Test

Step	Action
1	Take appropriate action to avoid a false trip
2	Provide NAMUR control signals to the Isolating Switching Amplifier to open/close the output and verify that the output is open/closed.
3	Restore the loop to full operation
4	Restore normal operation

This test will detect more than 90% of possible “du” failures of the Isolating Switching Amplifier.



Appendix 2: Impact of lifetime of critical components on the failure rate

Although a constant failure rate is assumed by the probabilistic estimation method (see section 4.2.3) this only applies provided that the useful lifetime of components is not exceeded. Beyond their useful lifetime, the result of the probabilistic calculation method is meaningless, as the probability of failure significantly increases with time. The useful lifetime is highly dependent on the component itself and its operating conditions – temperature in particular (for example, electrolyte capacitors can be very sensitive).

This assumption of a constant failure rate is based on the bathtub curve, which shows the typical behavior for electronic components.

Therefore it is obvious that the PFD_{AVG} calculation is only valid for components which have this constant domain and that the validity of the calculation is limited to the useful lifetime of each component.

It is assumed that early failures are detected to a huge percentage during the installation period and therefore the assumption of a constant failure rate during the useful lifetime is valid.

The circuits of the Isolating Switching Amplifiers IM1-**(Ex)-* and MK13-R-Ex0 do not contain any electrolytic capacitors or other components that are contributing to the dangerous undetected failure rate. Therefore there is no limiting factor with regard to the useful lifetime of the system.

However, according to section 7.4.7.4 of IEC 61508-2, a useful lifetime, based on experience, should be assumed. According to section 7.4.7.4 note 3 of IEC 61508-2 experience has shown that the useful lifetime often lies within a range of 8 to 12 years.

9 Turck Branches — Contact Data

Deutschland	Hans Turck GmbH & Co. KG Witzlebenstraße 7, 45472 Mülheim an der Ruhr www.turck.de
Australien	Turck Australia Pty Ltd Building 4, 19-25 Duerdin Street, Notting Hill, 3168 Victoria www.turck.com.au
Belgien	TURCK MULTIPROX Lion d'Orweg 12, B-9300 Aalst www.multiprox.be
Brasilien	Turck do Brasil Automação Ltda. Rua Anjo Custódio Nr. 42, Jardim Anália Franco, CEP 03358-040 São Paulo www.turck.com.br
China	Turck (Tianjin) Sensor Co. Ltd. 18,4th Xinghuazhi Road, Xiqing Economic Development Area, 300381 Tianjin www.turck.com.cn
Frankreich	TURCK BANNER S.A.S. 11 rue de Courtalin Bat C, Magny Le Hongre, F-77703 MARNE LA VALLEE Cedex 4 www.turckbanner.fr
Großbritannien	TURCK BANNER LIMITED Blenheim House, Hurricane Way, GB-SS11 8YT Wickford, Essex www.turckbanner.co.uk
Indien	TURCK India Automation Pvt. Ltd. 401-403 Aurum Avenue, Survey. No 109 /4, Near Cummins Complex, Baner-Balewadi Link Rd., 411045 Pune - Maharashtra www.turck.co.in
Italien	TURCK BANNER S.R.L. Via San Domenico 5, IT-20008 Bareggio (MI) www.turckbanner.it
Japan	TURCK Japan Corporation ISM Akihabara 1F, 1-24-2, Taito, Taito-ku, 110-0016 Tokyo www.turck.jp
Kanada	Turck Canada Inc. 140 Duffield Drive, CDN-Markham, Ontario L6G 1B5 www.turck.ca
Korea	Turck Korea Co, Ltd. A605, 43, Iljik-ro, Gwangmyeong-si 14353 Gyeonggi-do www.turck.kr
Malaysia	Turck Banner Malaysia Sdn Bhd Unit A-23A-08, Tower A, Pinnacle Petaling Jaya, Jalan Utara C, 46200 Petaling Jaya Selangor www.turckbanner.my

Mexiko	Turck Comercial, S. de RL de CV Blvd. Campestre No. 100, Parque Industrial SERVER, C.P. 25350 Arteaga, Coahuila www.turck.com.mx
Niederlande	Turck B. V. Ruiterlaan 7, NL-8019 BN Zwolle www.turck.nl
Österreich	Turck GmbH Graumanngasse 7/A5-1, A-1150 Wien www.turck.at
Polen	TURCK sp.z.o.o. Wroclawska 115, PL-45-836 Opole www.turck.pl
Rumänien	Turck Automation Romania SRL Str. Siriului nr. 6-8, Sector 1, RO-014354 Bucuresti www.turck.ro
Schweden	Turck AB Fabriksstråket 9, 433 76 Jonsered www.turck.se
Singapur	TURCK BANNER Singapore Pte. Ltd. 25 International Business Park, #04-75/77 (West Wing) German Centre, 609916 Singapore www.turckbanner.sg
Südafrika	Turck Banner (Pty) Ltd Boeing Road East, Bedfordview, ZA-2007 Johannesburg www.turckbanner.co.za
Tschechien	TURCK s.r.o. Na Brne 2065, CZ-500 06 Hradec Králové www.turck.cz
Türkei	Turck Otomasyon Ticaret Limited Sirketi Inönü mah. Kayisdagi c., Yesil Konak Evleri No: 178, A Blok D:4, 34755 Kadiköy/ Istanbul www.turck.com.tr
Ungarn	TURCK Hungary kft. Árpád fejedelem útja 26-28., Óbuda Gate, 2. em., H-1023 Budapest www.turck.hu
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